



CONTROL OF CHAOS IN SPROTT SYSTEM B BY STATE SPACE EXACT LINEARIZATION METHOD

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Abstract In this communication, a non-linear chaotic dynamical system has been transferred into a linear controllable system using state space exact linearization method via lie algebra. Numerical simulation is applied to justify our claim.

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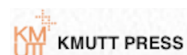
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1. INTRODUCTION

In 1998, the state space exact linearization (SSEL) method for non-linear control system [4] is introduced by Liqun and Yanzhu [1]. They considered the very famous Lorenz dynamical system [5, 6] and applied their method. Here we consider Sprott's chaotic non-linear dynamical system B. This system has two non-linear terms with one non-zero

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parameter. To control the chaotic Sprott system B, we are applying the previously mentioned SSEL method via lie algebra, which transformed the non-linear dynamical system into a linear controllable system.

2. THE EXACT LINEARIZATION METHOD

Let us consider two smooth functions $f : \mathbb{R}^n \rightarrow \mathbb{R}^n$ and $g : \mathbb{R}^n \rightarrow \mathbb{R}^n$ which are also smooth vector fields on \mathbb{R}^n .

Let $x \in \mathbb{R}^n$ and $u \in \mathbb{R}^1$ be the state variable and control parameter respectively. Then, any single-input non-linear system can be taken as

$$\dot{x} = f(x) + ug(x) \quad (2.1)$$

Let $[X, Y]$ be the Lie bracket of vector fields X and Y. Let us denote

$$ad_f^i g(x) = [f, ad_f^{i-1} g](x), \quad i \geq 1 \quad (2.2)$$

with $ad_f^0 g(x) = g(x)$.

If $f = [f_1, f_2, f_3, \dots, f_n]^T$ and $g = [g_1, g_2, g_3, \dots, g_n]^T$, using Lie-algebra, we may consider

$$ad_f^i g = [(ad_f^i g)_1, (ad_f^i g)_2, (ad_f^i g)_3, \dots, (ad_f^i g)_n]^T, \quad (2.3)$$

where

$$(ad_f^i g)_j = \sum_{k=1}^n \left\{ f_k \frac{\partial (ad_f^{i-1} g)_j}{\partial x_k} - (ad_f^{i-1} g)_k \frac{\partial f_j}{\partial x_k} \right\}, \quad j = 1, 2, 3, \dots, n \text{ and } i \geq 1 \quad (2.4)$$

Let $L_X \lambda$ denote the Lie derivative of the real-valued function $\lambda(x)$ with respect to the vector field X.

Then, in a neighbourhood $N(x_0)$ of x_0 , one can easily obtain the relations

$$L_g \lambda(x) = L_{ad_f^1 g} \lambda(x) = \dots = L_{ad_f^{n-2} g} \lambda(x) = 0$$

and

$$L_{ad_f^{n-1} g} \lambda(x_0) \neq 0, \quad x \in N(x_0) \quad (2.5)$$

if the following two conditions are satisfied :

- 1) Rank of $\Delta = n$, where $\Delta = [g(x_0), ad_f^1 g(x_0), \dots, ad_f^{n-1} g(x_0)]$ and
- 2) Γ is involutive, where $\Gamma = span\{g, ad_f^1 g, ad_f^2 g, \dots, ad_f^{n-2} g\}$, near x_0 .

Moreover, in the neighbourhood $N(x_0)$ of x_0 , there exists the transformation

$$\begin{aligned} z &= [z_1, z_2, z_3, \dots, z_n]^T \\ &= \Psi(x) \\ &= [\Psi_1(x), \Psi_2(x), \Psi_3(x), \dots, \Psi_n(x)]^T \\ &= [\lambda(x), L_f \lambda(x), L_f^2 \lambda(x), \dots, L_f^{n-1} \lambda(x)]^T \end{aligned} \quad (2.6)$$

and

$$w = b(x) + ua(x) \quad (2.7)$$

where $a(x) = L_g L_f^{n-1} \lambda(x)$ and $b(x) = L_f^n \lambda(x)$.

Hence, we get the linear controllable system [2] from the non-linear system (2.1) by the SSEL method as given below :

$$\dot{z}_1 = z_2, \quad \dot{z}_2 = z_3, \quad \dot{z}_3 = z_4, \dots, \quad \dot{z}_{n-1} = z_n, \quad \dot{z}_n = w.$$

3. CONTROL OF THE SPROTT MODEL B

The Sprott's non-linear chaotical dynamical system [3] is given by

$$\begin{aligned} \dot{x}_1 &= x_2 x_3 \\ \dot{x}_2 &= x_1 - x_2 \\ \dot{x}_3 &= \gamma - x_1 x_2 \end{aligned} \quad (3.1)$$

where $\gamma (\neq 0)$ is a parameter.

This system can be written as

$$\dot{x} = f(x) + ug(x)$$

where $f(x_1, x_2, x_3) = [x_2 x_3, x_1 - x_2, \gamma - x_1 x_2]^T$, $x \in \mathbb{R}^3$,

$g(x_1, x_2, x_3) = [0, x_1, 0]^T$, $u = u(x_1, x_2, x_3)$.

To make the linear controllable system using state space exact linearization method, we have to verify the two conditions as discussed earlier :

1) Rank of $\Delta = 3$, where $\Delta = [g, ad_f^1 g, ad_f^2 g]$ and

2) Γ is involutive, where $\Gamma = span\{g, ad_f^1 g\}$.

Now, using (2.2), (2.3) and (2.4),

$$[f, g] = ad_f^1 g = [(ad_f^1 g)_1, (ad_f^1 g)_2, (ad_f^1 g)_3]^T = [-x_1 x_3, x_2 x_3 + x_1, x_1^2]^T$$

Again, by similar process, we have,

$$[f, ad_f^1 g] = ad_f^2 g = \begin{bmatrix} -2x_2 x_3^2 - x_1 x_3 - \gamma x_1 \\ x_2 x_3 + 2x_1 x_3 + x_1 + \gamma x_2 - x_1 x_2^2 \\ 2x_1 x_2 x_3 + x_1^2 \end{bmatrix}$$

So, if $x_1 \neq 0$,

$$|\Delta| = \begin{vmatrix} 0 & -x_1 x_3 & -2x_2 x_3^2 - x_1 x_3 - \gamma x_1 \\ x_1 & x_2 x_3 + x_1 & x_2 x_3 + 2x_1 x_3 + x_1 + \gamma x_2 - x_1 x_2^2 \\ 0 & x_1^2 & 2x_1 x_2 x_3 + x_1^2 \end{vmatrix} = -\gamma x_1^4 \neq 0,$$

\therefore We can say, Rank of $\Delta = 3$.

Now, $(g, ad_f^1 g)_1 = 0$, $(g, ad_f^1 g)_2 = 2x_1 x_3$, $(g, ad_f^1 g)_3 = 0$.

Hence, $[g, ad_f^1 g] = [0, 2x_1 x_3, 0]^T$.

\therefore it is similar like g as $[g, ad_f^1 g]$ is along the y-axis.

Thus, $\Gamma = span\{g, ad_f^1 g\}$ which is involutive, where $x_i \in \mathbb{R}$, $i = 1, 2, 3$.

Hence, the required two conditions for the relation (2.5) have been satisfied for $n = 3$.

Now, $L_g \lambda(x) = 0$ gives $x_1 \frac{\partial \lambda}{\partial x_2} = 0$.

This implies that

$$\frac{\partial \lambda}{\partial x_2} = 0 \quad \text{as } x_1 \neq 0 \quad (3.2)$$

$L_{ad_f^1 g} \lambda(x) = 0$ gives

$$\begin{aligned} -x_1 x_3 \frac{\partial \lambda}{\partial x_1} + x_1^2 \frac{\partial \lambda}{\partial x_3} &= 0 \\ \text{or, } x_3 \frac{\partial \lambda}{\partial x_1} - x_1 \frac{\partial \lambda}{\partial x_3} &= 0 \quad \text{as } x_1 \neq 0 \end{aligned} \quad (3.3)$$

Then, solution of the equation (3.3) is given by,

$$\lambda = x_1^2 + x_3^2 + \sigma \quad (3.4)$$

where σ is a numerical constant chosen in such way that the goal of the control can be attained.

Since $\frac{\partial \lambda}{\partial x_2} = 0$, using (3.3), we can write $L_{ad_f^2 g} \lambda(x)$ as

$$\begin{aligned} L_{ad_f^2 g} \lambda(x) &= (ad_f^2 g)_1 \frac{\partial \lambda}{\partial x_1} + (ad_f^2 g)_3 \frac{\partial \lambda}{\partial x_3} \\ &= -\frac{\gamma x_1^2}{x_3} \frac{\partial \lambda}{\partial x_3} \\ &= -2\gamma x_1^2 \\ &\neq 0, \quad \text{since } x_1 \neq 0 \quad \text{and } \gamma \neq 0 \end{aligned} \quad (3.5)$$

Using (3.4), we have,

$$L_f \lambda(x) = 2\gamma x_3 \quad (3.6)$$

and

$$\begin{aligned} L_f^2 \lambda(x) &= L_f(L_f \lambda(x)) \\ &= x_2 x_3 \frac{\partial}{\partial x_1} (L_f \lambda(x)) + (x_1 - x_2) \frac{\partial}{\partial x_2} (L_f \lambda(x)) + (\gamma - x_1 x_2) \frac{\partial}{\partial x_3} (L_f \lambda(x)) \\ &= 2\gamma(\gamma - x_1 x_2) \end{aligned} \quad (3.7)$$

According to the state space exact linearization method, using (2.6) we can construct the transformation process as given below:

$$\begin{aligned} z &= [z_1, z_2, z_3]^T \\ &= \Psi(x) \\ &= [\Psi_1(x), \Psi_2(x), \Psi_3(x)]^T \\ &= [\lambda(x), L_f^1 \lambda(x), L_f^2 \lambda(x)]^T \end{aligned}$$

and

$$w = b(x) + ua(x) \quad (3.8)$$

where

$$a(x) = L_g L_f^2 \lambda(x) \quad \text{and} \quad b(x) = L_f^3 \lambda(x). \quad (3.9)$$

Hence,

$$\begin{bmatrix} z_1 \\ z_2 \\ z_3 \end{bmatrix} = z = \Psi(x) = \begin{bmatrix} x_1^2 + x_3^2 + \sigma \\ 2\gamma x_3 \\ 2\gamma(\gamma - x_1 x_2) \end{bmatrix} \quad (3.10)$$

From (3.10), we can construct the inverse transformation as

$$\begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} = x = \Psi^{-1}(z) = \begin{bmatrix} \frac{\sqrt{4\gamma^2 z_1 - 4\gamma^2 \sigma - z_2^2}}{2\gamma} \\ \frac{2\gamma^2 - z_3}{\sqrt{4\gamma^2 z_1 - 4\gamma^2 \sigma - z_2^2}} \\ \frac{z_2}{2\gamma} \end{bmatrix} \quad (3.11)$$

From (3.9), we have,

$$\begin{aligned} a(x) &= L_g L_f^2 \lambda(x) \\ &= x_1 \frac{\partial}{\partial x_2} (L_f^2 \lambda(x)) \\ &= -2\gamma x_1^2 \end{aligned} \quad (3.12)$$

$$\begin{aligned} b(x) &= L_f^3 \lambda(x) \\ &= x_2 x_3 \frac{\partial}{\partial x_1} (L_f^2 \lambda(x)) + (x_1 - x_2) \frac{\partial}{\partial x_2} (L_f^2 \lambda(x)) + (\gamma - x_1 x_2) \frac{\partial}{\partial x_3} (L_f^2 \lambda(x)) \\ &= -2\gamma x_2^2 x_3 - 2\gamma x_1^2 + 2\gamma x_1 x_2 \end{aligned} \quad (3.13)$$

∴ From (3.8), u can be obtained as

$$\begin{aligned} u &= \frac{w}{a(x)} - \frac{b(x)}{a(x)} \\ \text{or, } u &= -\frac{w}{2\gamma x_1^2} - \frac{x_2^2 x_3 + x_1^2 - x_1 x_2}{x_1^2} \end{aligned} \quad (3.14)$$

Using (3.8) and [(3.10) - (3.13)], we have got the linear controllable system from the system of equation (3.1) as given below:

$$\dot{z}_1 = z_2, \quad \dot{z}_2 = z_3 \quad \text{and} \quad \dot{z}_3 = w \quad (3.15)$$

where w can be taken as

$$w = c_1 z_1 + c_2 z_2 + c_3 z_3 \quad (3.16)$$

in such way that by changing the value of σ , we can control the variable x_1 to the goal x_g .

Using (3.10) and (3.16) in (3.14), one gets,

$$\begin{aligned} u &= -\frac{c_1(x_1^2 + x_3^2 + \sigma) + 2c_2\gamma x_3 + 2c_3\gamma(\gamma - x_1 x_2)}{2\gamma x_1^2} \\ &\quad - \frac{x_2^2 x_3 + x_1^2 - x_1 x_2}{x_1^2} \end{aligned} \quad (3.17)$$

which gives the linear feedback control parameter u .

With the help of (3.11), we may consider the term σ as given below :

$$\sigma = -x_g^2 \quad (3.18)$$

where x_g is the control goal.

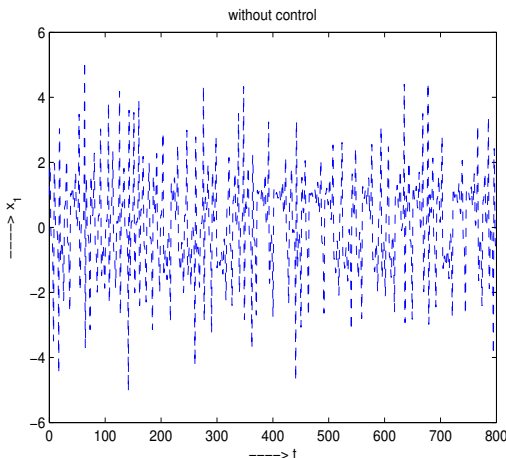


FIGURE 1. The time evolution of x_1 in uncontrolled system

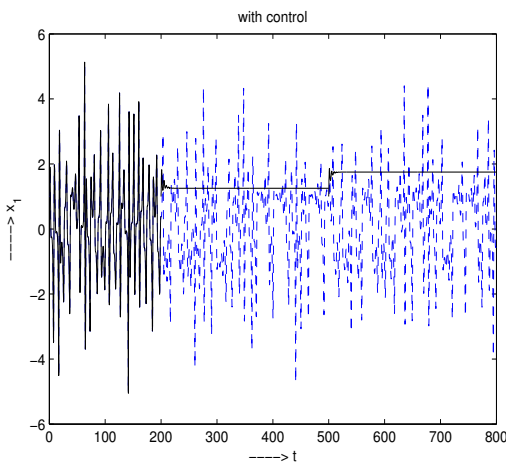


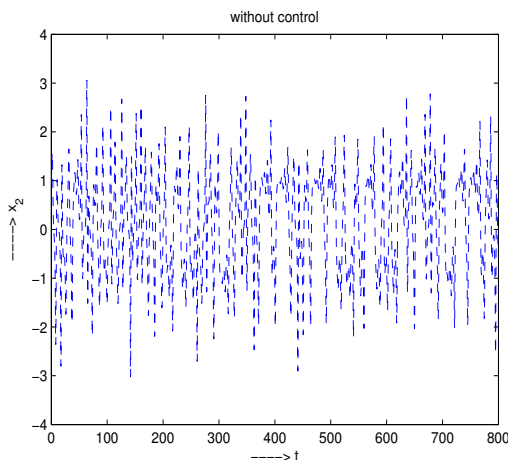
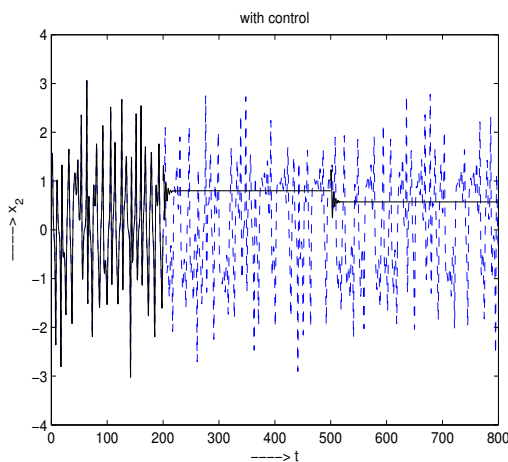
FIGURE 2. The time evolution of x_1 in controlled system

4. RESULTS AND DISCUSSIONS

For $\gamma = 1$, Sprott found that the system (3.1) is chaotic. Numerical simulation is done with the initial values of the state variables $x_1(0) = 1, x_2(0) = 1$ & $x_3(0) = 1$. For the controlled system (3.15), the parameters c_1, c_2, c_3 are chosen[7] in such way that $c_1 + c_2c_3 > 0$ with $c_1 < 0, c_2 < 0$ & $c_3 < 0$ are satisfied.

Here, we have taken $c_1 = -0.5, c_2 = -2.5$ & $c_3 = -0.75$ and the control is started at $t = 200$ with $x_g = 1.25$. At time $t = 500$, the control goal is changed from $x_g = 1.25$ to $x_g = 1.75$.

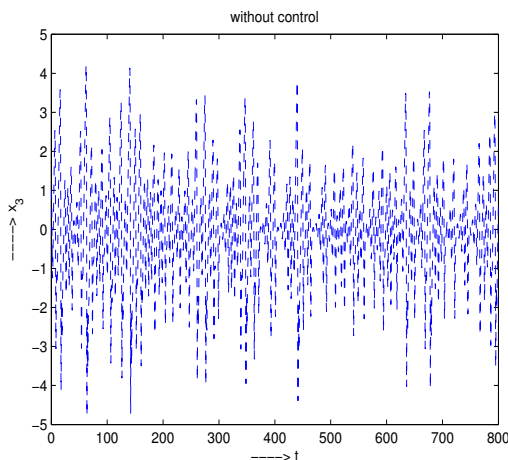
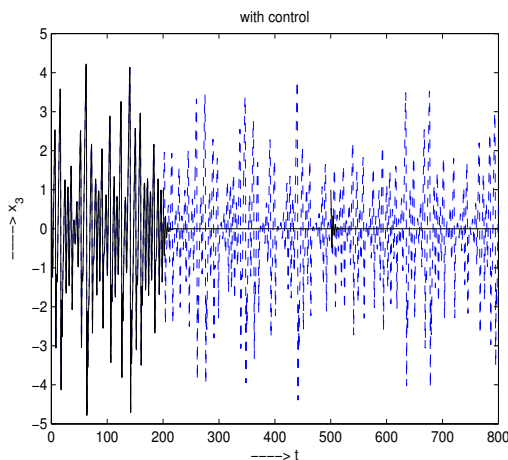
Using Runge-Kutta method, time evolution of x_1, x_2, x_3 are shown in the figure(1), figure(3) and figure(5) respectively with $u = 0$ whereas figure(2), figure(4) and figure(6)

FIGURE 3. The time evolution of x_2 in uncontrolled systemFIGURE 4. The time evolution of x_2 in controlled system

depict the time evolution of x_1, x_2, x_3 respectively in presence of control u . Finally, we conclude that the SSEL method has been applied successfully to control the Sprott system B.

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FIGURE 5. The time evolution of x_3 in uncontrolled systemFIGURE 6. The time evolution of x_3 in controlled system

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